

LICE

# HIE-ISOLDE Cryomodule Thermal Analysis – 1<sup>st</sup> part

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ATIAS

**CERN** Prévessin

# Agenda



1	Introduction
2	Objective
3	HIE-ISOLDE: FEM Model
4	HIE-ISOLDE: Model checks
5	Thermal steady-state analysis
6	Thermal transient analysis
7	Advanced thermal analysis
8	Conclusions and next steps



# Introduction



- □ High Intensity and Energy ISOLDE
- **Current state**
- **G** Future phases





# Objective



- Global temperature and heat flux mapping
- Design validation
- Advanced thermal analysis



## Targets:

- 1. Global temperature and heat flux mapping
- 2. Validation of the experimental tests
- 3. Simulation tool for future thermo-mechanical analysis



# Outline



1	HIE-ISOLDE: cryomodule
2	Analytical heat loads estimation
3	FEM model
4	Model checks
5	Thermal steady-state analysis
6	Conclusions and next steps



# **HIE-ISOLDE:** Main components

## Vacuum vessel

Interfaces

## Top plate

- Seal interface
- Thermal shield
  - Cryogenics circuit

## Helium reservoir

- Cryogenics piping
- Cryogenics supply

## Supporting frame assembly

- Actively cooled frame
- Suspension rods
- Adjustment mechanisms

## 5 QWR cavities

- RF supply and pick-up
- Tuner and coupler motors

## 1 solenoid

- Protection system
- Current leads







# **HIE-ISOLDE:** Procedure



## 1. Initial status

300K structures

## 2. Thermal shield cool down

- 300K-75K
- 13 bar

## 3. Reservoir + frame cool down

- 300K-75K
- 2.5 bar

## 4. Reservoir + frame cool down

- **75K-4.5K**
- 2.5 bar

## 5. Global cool down

- Thermal shield circuit : 13barG, 55-75K
- Cold mass circuits: 1.3 barG, 4.5K





# **HIE-ISOLDE: 55K-70K GHe circuit**



Characteristics:

- 55K-70K gaseous helium
- 13 bar nominal





# **HIE-ISOLDE: 4.5K LHe-GHe circuit**



## Characteristics:

- 2.5 bar transient
- 1.3 bar nominal





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# **Analytical heat loads estimation**





$$\dot{q} = -\frac{A}{L} \int_{Tcold}^{Twarm} k(T) dT$$

□ radiation

$$q_{w-c} = \frac{\sigma \left( T_{warm}^4 - T_{cold}^4 \right)}{\frac{1 - \varepsilon_w}{\varepsilon_w A_w} + \frac{1}{A_w F} + \frac{1 - \varepsilon_c}{\varepsilon_c A_c}}$$

convection

 $Q = hA_{tr}\Delta T$ h = Nu.k/d $Nu = \alpha Re^{0.8} Pr^{n}$  $Re = \frac{4Q_m}{\pi d\mu}$  $Pr = \frac{Cp.\mu}{k}$ 





# **HIE-ISOLDE: 55K-70K GHe circuit**



#### Heat loads estimation of the 55K-70K GHe circuit

Heat	Source	Value [W]	With margin [W]
Radiation	Radiative heat exchange VV vs. TS	190	350
	Thermal shield supports	10	20
	Reservoir thermalization	58	58
	Tie-rods thermalization	9	9
	RF cables thermalization	15	25
Conduction	RF pick-up	15	15
	Tuner-coupler rods	4	4
	GHE Bayonets (CM side)	3	6
	Solenoid adjusting rods	1	1
	Instrumentation	7	10
Dynamic	RF cables thermalization	52	52
tot.		364	550





# **HIE-ISOLDE: 4.5K LHe-GHe circuit**



#### Heat loads estimation of the 4.5K LHe-GHe circuit

Heat	Source	Value [W]	With margin
	Radiative heat exchange TS vs. CM	0.57	0.81
Dediation	Beam port openings	0.83	0.83
Radiation	Viewports openings	0.2	0.3
	Gap around the TS lid	0.3	0.45
	Reservoir thermalization	6.1	6.1
	Tie-rods thermalization	0.2	0.2
	RF supply cables	1	2.5
	RF pick-up cables	1	2.5
Conduction	Tuner-coupler rods	0.1	0.1
	Bayonets (CM side)	6.1	12.2
	Solenoid adjusting rods	0.03	0.03
	Instrumentation low current	0.4	0.4
	Instrumentation heaters	1.3	1.3
Dunamic	Coupler	2	5
Dynamic	Cavities	50	50
tot.		70	82



+ liquefaction load



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# **FEM Model**



## **Complexity of geometry**

- Number of components
- Connections

## **Complexity of thermal phenomena**

- Wide temperature range (4.5K-300K)
- Internal forced helium flow
- Radiation

## **Targets of FEM analysis:**

- 1. Global temperature and heat flux mapping
- 2. Validation of the experimental tests
- 3. Simulation tool for future thermo-mechanical analysis







- Vacuum vessel
- Top plate
- Thermal shield
  - Cryogenics circuit
- Supporting frame assembly
  - Actively cooled frame
  - Suspension rods
- Helium reservoir
  - Cryogenics piping
- 5 cavities
- 1 solenoid



Vacuum vessel: -15 mm (40mm) thick plates -316L polished -4.5 T welded assembly



- Vacuum vessel
- Top plate
- Thermal shield
  - Cryogenics circuit
- Supporting frame assembly
  - Actively cooled frame
  - Suspension rods
- Helium reservoir
  - Cryogenics piping
- □ 5 cavities
- 1 solenoid





#### -300 kg bolted assembly -2 mm thick Cu Ni-plated

**Thermal Shield :** -2.2m x 1.8m x 0.9m

-Piping : GHe 70K, 13 bara -No porosities after brazing



- Vacuum vessel
- Top plate
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- Supporting frame assembly
  - Actively cooled frame
  - Suspension rods
- Helium reservoir
  - Cryogenics piping
- □ 5 cavities
- 1 solenoid





Supporting frame : -2.1m x 0.4m x 0.4m -316L, electro-polished -130 kg welded assembly -Piping : LHe 4.5K, 4.5 bara



- Vacuum vessel
- Top plate
- Thermal shield
  - Cryogenics circuit
- Supporting frame assembly
  - Actively cooled frame
  - Suspension rods
- □ Helium reservoir
  - Cryogenics piping
- □ 5 cavities
- 1 solenoid



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- Vacuum vessel
- Top plate
- Thermal shield
  - Cryogenics circuit
- Supporting frame assembly
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  - Suspension rods
- Helium reservoir
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- **5** cavities
- **1** solenoid





- Vacuum vessel
- Top plate
- **Thermal shield** 
  - Cryogenics circuit н.
- □ Supporting frame assembly
  - Actively cooled frame
  - Suspension rods

#### Helium reservoir

- Cryogenics piping
- **5** cavities
- 1 solenoid





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4 5	Model checks Thermal steady-state analysis
4 5 6	Model checks Thermal steady-state analysis Conclusions and next steps



## **Finite Element Model (source ESA/ECSS standards):**

- Geometry
- Mesh
- Loads
- Rigid body motion







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## Finite Element Model (source ESA/ECSS standards):

## Model geometry

- ✓ Mass (components, total)
- ✓ Centre of gravity (with common SoR)
- ✓ Moments of inertia
- ✓ Contacts (around n. 300)



Tra	nslational mas	3	1	Coupled trans	lational/rotat:	ional mass
0.29976	0.0000	0.0000	i.	0.0000	-300.12	13.345
0.0000	0.29976	0.0000	- i	300.12	0.0000	0.55811
0.0000	0.0000	0.29976	1	-13.345	-0.55811	0.0000
			•   •	Rotatio	nal mass (iner	tia)
			- i -	0.46185E+06	176.57	1278.1
			- i	176.57	0.58399E+06	-12322.
			1	1278.1	-12322.	0.19057E+
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Bounding Box			
Length X	2188.4 mm		
Length Y	886. mm		
Length Z	1991. mm		
	Properties		
Volume	3.6088e+007 mm <sup>s</sup>		
Mass	299.53 kg		



# CERN

## Finite Element Model (source ESA/ECSS standards):

## Element topology

- <u>Aspect ratio</u>: max. edge length /min edge length;
- Jacobian ratio: measure of the deviation of a given element from an ideally shaped element;
- ✓ <u>Warping factor</u>: warp angle is the out of plane angle;
- ✓ <u>Skewness</u>: minimum angle between two lines joining opposite midsides of the element;
- ✓ <u>Convergence</u> of mesh refinement;

### Nodes: 283,005

*Elements: 113,146* 

	min	max	average	st.dev.	ideal
Aspect ratio	1.03	25.97	1.45	0.6	1
Jacobian ratio	0.45	49.81	1.08	0.4	1
Warping factor	0	1.44E-14	3.43E-15	0	0
Skewness	3.91E-03	0.99	0.21	0.1	0





## Finite Element Model (source ESA/ECSS standards)

## Static analysis

- ✓ Unit load check
- ✓ Load resultants
- ✓ Residual load vector
- ✓ No internal mechanism

## **Gamma** Stress free thermo-elastic deformation

✓ Uniform temperature decrease



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## Finite Element Model (source ESA/ECSS standards):

## Static analysis

- ✓ Unit load check
- ✓ Load resultants
- ✓ Residual load vector
- ✓ No internal mechanism

## **G** Stress free thermo-elastic deformation

✓ Uniform temperature decrease



10e-4



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# Outline



1	HIE-ISOLDE: cryomodule
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5	Thermal steady-state analysis



# Thermal steady-state analysis (1/2)



a radiation a conduction adynamic



- Emissivity
  - Vacuum vessel: 0.2
  - Thermal shield: [0.033,0.066]

$$\dot{q}_{1\to 2} = \dot{q}_1 = -\dot{q}_2 = \frac{\sigma(T_1^4 - T_2^4)}{\frac{1 - \varepsilon_1}{\varepsilon_1 A_1} + \frac{1}{A_1 F_{12}} + \frac{1 - \varepsilon_2}{\varepsilon_2 A_2}}$$





emissivity of TS

# Thermal steady-state analysis (2/2)



## OB: Temperature mapping inside the CM













# Thermalisation (1/2)

OB: determine the efficiency of the two copper stripes on cooling down of the oblique rod supporting the frame. The results are compared to an alternative option with just a single thermalisation.

Hp1: Isotropic coefficient of thermal expansion function of temperature











# Thermalisation (2/2)

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- □ Single thermalisation has an important effect only in case of pure conduction heat transfer increasing the time to reach T(max)<100K from 50 to 65 hours;
- □ In the conduction + radiation model (realistic case) this effect is less important due to the influence of the radiation;

#### With radiation







	Two thermalisations	One thermalisation
Only conduction	50 h	65 h
Conduction + radiation	21 h	23 h



# Outline



6	Conclusions and next steps
5	Thermal steady-state analysis
4	Model checks
3	FEM model
2	Analytical heat loads estimation
1	HIE-ISOLDE: cryomodule



# Conclusions



## □ Thermal network;

- General analytical estimation of heat loads inside the cryomodule updated version;
- □ FEM model validated with the ECSS standards;
- Global thermal steady state analysis;

## Next:

- Global radiation analysis need for emissivity values in cryogenic conditions;
- □ Increase complexity of geometry;



# ... in the next episode



- Thermal transient analysis 1.
- Advanced thermal analysis: 2.
  - Frame support and cryogenic circuit;

197.78 172.22 146.67 121.11

- Omega plates;
- Vacuum Vessel cleaning;
- RF cable;
- Solenoid splices.







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- [3] D. Ramos, "Radiation heat exchange in the HIE-ISOLDE cryomodule," CERN, 2013-08-01.
- [4] L. Williams, "Cryostat for HIE-ISOLDE high energy cryomodule," CERN, 2010-06-17.



## Instrumentation





